

# Modelling and Evaluation of the Thermohydraulic Performance of Finned-Tube Supercritical Carbon Dioxide Gas Coolers

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## **1. INTRODUCTION**

Supercritical carbon dioxide (sCO<sub>2</sub>) is becoming an important commercial and industrial fluid due to its environmental credentials and its advantageous characteristics, such as being nontoxic and non-flammable and having low viscosity and a large refrigeration capacity. Thermodynamic systems using sCO<sub>2</sub> as the working fluid have been widely studied in many engineering applications, such as refrigeration and heat pumps, and power generation and conversion systems. In these systems, the thermohydraulic performance of gas coolers has a significant influence on the system efficiency. The understanding of the thermohydraulic performance under different operating conditions is essential for design and optimization purposes. To achieve this objective, Yin et al. [1] and Asinari et al. [2], respectively developed a first principles-based model and a fully three-dimensional simulation model for microchannel gas coolers. Ge et al. [3], Gupta et al. [4], Marcinichen et al. [5] and Singh et al. [6] proposed detailed mathematical models utilizing distributed methods for finned-tube gas coolers. Li et al. [7, 8] developed a simplified mathematical model for an air-cooled coil gas cooler. In this paper, a detailed mathematical model employing the distributed method is discussed, and the thermohydraulic performance of two finned-tube sCO<sub>2</sub> gas coolers [9], is investigated.

## 2. METHDOLOGY

Figure 1 demonstrates the distributed method (segment by segment) design for the two finned-tube  $sCO_2$  gas coolers. Gas cooler A has 3 tube rows with 8 tubes per row, and gas cooler B, 2 tube rows, and 16 tubes per row. The finned copper tubes have 8 mm outer diameter, 0.68 mm wall thickness and 1.6 m length. The thickness of the wavy aluminum fins is 0.16 mm and the fin spacing 2.12 mm. For the model, each tube is divided into 20 equal segments. For each segment, the  $\varepsilon$ -NTU method [10] is employed for the heat transfer and pressure drop calculations. The thermophysical properties of the sCO<sub>2</sub> and the cooling air in each segment using the NIST REFPROP v9.1 software.



Fig. 1 Model of finned-tube sCO<sub>2</sub> gas cooler: (a) gas cooler A, and (b) gas cooler B.

The thermohydraulic performance of the fluid flowing over or through the tubes is calculated using empirical correlations for Nusselt number and friction factor: Krasnoshchekov and Protopopov [11] correlation for  $sCO_2$  and Wang et al. [12] correlation for cooling air. Since the density of  $sCO_2$  undergoes a significant change with temperature in the near-critical region, the pressure drop of  $sCO_2$  takes into consideration the influence of flow deceleration.

## **3. RESULTS**

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The models were verified against the experimental data from Santosa et al. [9]. The comparison between the modelling predictions and the experimental results is illustrated in Table 1. Considering the uncertainty of the K-type thermocouples and pressure transducers used in the test facility, the present modelling can predict the thermohydraulic performance of the gas coolers with good accuracy. For numbers 1-6, the sCO<sub>2</sub> pressure drop from the modelling  $\Delta P_{ref}$ , mol are 12.5, 11.4, 11.8, 52.3, 66.2 and 70.7 kPa. Gas cooler B shows much larger pressure drop but similar heat transfer rate for per unit mass flow rate of sCO<sub>2</sub> compared to gas cooler A with the other similar operating conditions, due to the different engineering design.

	<b>Operating condition</b>					Results					
Test	Vair, in	Tair, in	$P_{ m ref,\ in}$	$T_{\rm ref, in}$	$m_{\rm ref}$	$\Delta P_{\rm air, exp}$	$\varDelta P_{ m air,\ mol}$	$T_{\rm ref, out, exp}$	$T_{\rm ref, out, mol}$	$Q_{\exp}$	$Q_{ m mol}$
	(m/s)	(°C)	(bar)	(°C)	(kg/s)	(Pa)	(Pa)	(°C)	(°C)	(kW)	(kW)
	Gas cooler A					Gas cooler A					
No. 1	1.7	32.8	85.1	105.5	0.0105	26.6	26.9	33.2	32.83	2.4	2.46
No. 2	2.0	32.8	84.2	99.2	0.01	34.2	34.8	32.8	32.82	2.23	2.31
No. 3	2.4	34.3	86.6	116.8	0.0103	41.4	46.6	34.9	34.31	2.4	2.43
	Gas cooler B					Gas cooler B					
No. 4	1.7	35.1	86.3	100.8	0.019	13.9	17.6	35.3	35.38	4.1	4.12
No. 5	2.0	35.2	86.5	104.6	0.0215	25.6	22.7	35.0	35.54	4.6	4.75
No. 6	2.4	33.0	83.9	101.3	0.021	27.6	30.4	33.0	33.15	4.65	4.94

Table 1 Comparison of modelling results with experiment data

Following model verification, the effect of sCO<sub>2</sub> mass flow rate  $m_{ref}$  on the thermohydraulic performance was investigated. For gas cooler A and test No. 3 increasing the  $m_{ref}$  by 100% increased the sCO<sub>2</sub> outlet temperature  $T_{ref, out, mol}$  from 34.3 °C to 35.0 °C, and the heat transfer rate  $Q_{mol}$  from 2.43 kW to 4.9 kW.  $\Delta P_{ref, mol}$  increases by 4 times from 11.8 kPa to 47.1 kPa. For gas cooler B and test No. 6 doubling  $m_{ref}$  increased  $T_{ref, out, mol}$  from 33.2 °C to 35.3 °C, and  $Q_{mol}$  from 4.9 kW to 8.7 kW. The pressure drop  $\Delta P_{ref, mol}$  quadruples from 70.7 kPa to 282.4 kPa.

The higher pressure drop in gas cooler B is due to the higher mass flow rate and total length of tubes in each row of the gas cooler. Even though the heat transfer for per unit mass flow rate is similar to gas cooler A, the higher pressure drop will lead to a higher compressor power consumption which will impact on the overall efficiency of the  $CO_2$  refrigeration system.

### 4. CONCLUSIONS

To investigate the thermohydraulic performance of finned-tube sCO<sub>2</sub> gas coolers, a detailed mathematical model employing the distributed modelling approach and the  $\varepsilon$ -NTU method was developed and presented in this study. The model uses empirical correlations for the Nusselt number and friction factor for the heat transfer and pressure drop calculations on the sCO<sub>2</sub> and cooling air sides. The model was validated against experimental data and then employed to investigate the influence of design and operating parameters on overall gas cooler performance. The pressure drop in the gas cooler is an important parameter in the optimization of the performance of CO<sub>2</sub> refrigeration and heat pump systems particularly in the drive to reduce the footprint of components and the system as a whole. The model will be used as a tool in the investigation of the potential of 5.0 mm tube and microchannel heat exchangers as CO<sub>2</sub> gas coolers.

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